



The PETRA III Girder concept

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Girder concept



Accuracy requirements:

magnet to magnet on girder $\sigma = 50\mu\text{m}$

girder to girder $\sigma = 100\mu\text{m}$

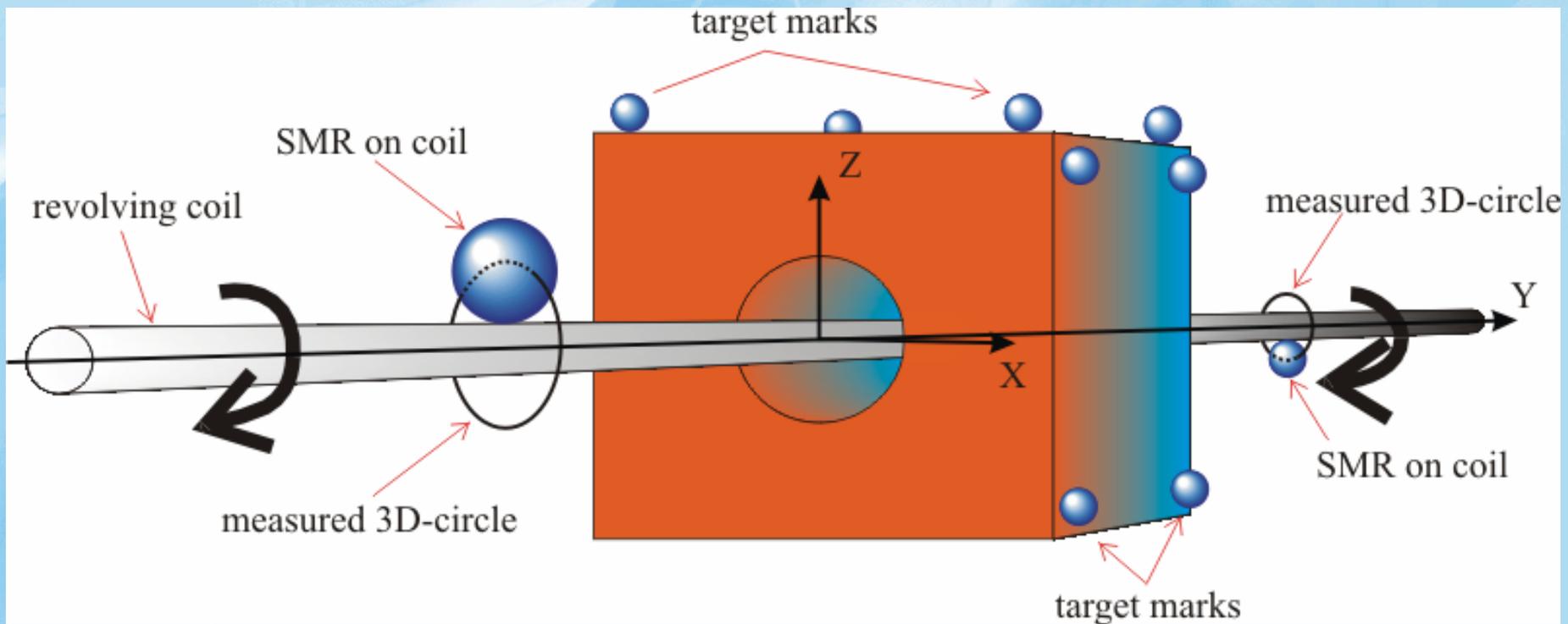
both in lateral and height



Transfer measurement



Task: Transfer magnetic axis to target marks



Transfer measurement

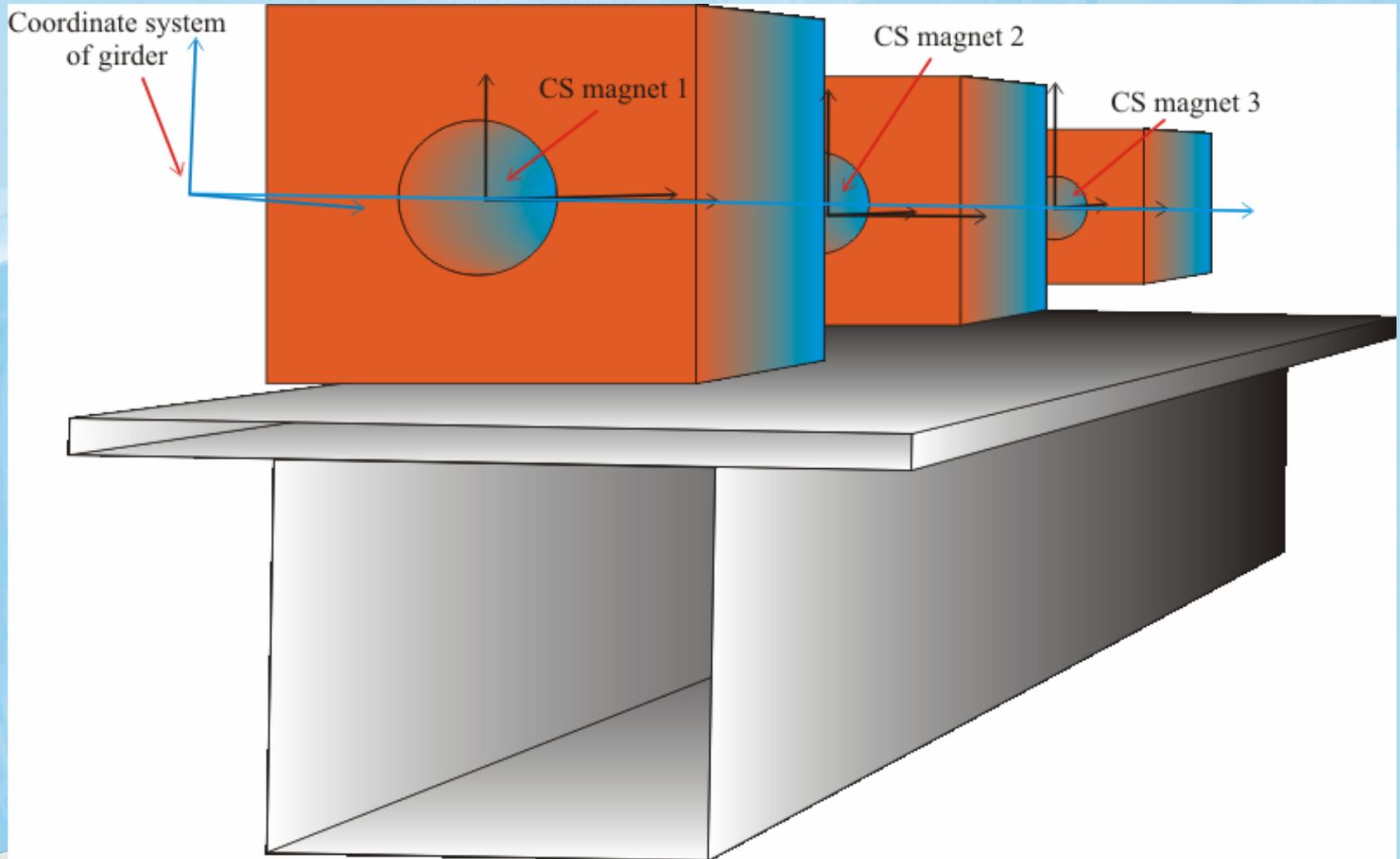


- magnetic axis determined by $\sigma = 5\mu\text{m}$
- revolving SMR defines circle
- circle is measured by tracker
- center of circle better than $\sigma = 5\mu\text{m}$
- measurement to target marks with $\sigma = 20\mu\text{m}$

gives us $\sigma = 21\mu\text{m}$ for transfer measurement



Alignment of magnets on girder



Alignment of magnets on girder



- CS of girder is oriented roughly to the mechanical structure of girder
- all magnets are aligned to this system by three rotations and translations
- movements done by DESY-standard elements (ballshaped screws & turnbuckles)
- accuracy comes from measurement ($\sigma = 20\mu\text{m}$) and from adjustment ($\sigma = 10\mu\text{m}$)

gives us $\sigma = 22\mu\text{m}$ for alignment on girder



Intra-girder accuracy



Magnet to magnet accuracy results from

- transfer measurement accuracy
- alignment accuracy

$$\sigma_{mm} = 30\mu m$$

... but only if ideal conditions are met:

- climatized room
 - good geometry
 - precisely calibrated instruments, etc.
- can not be done in tunnel



Transport



everything would be great ...

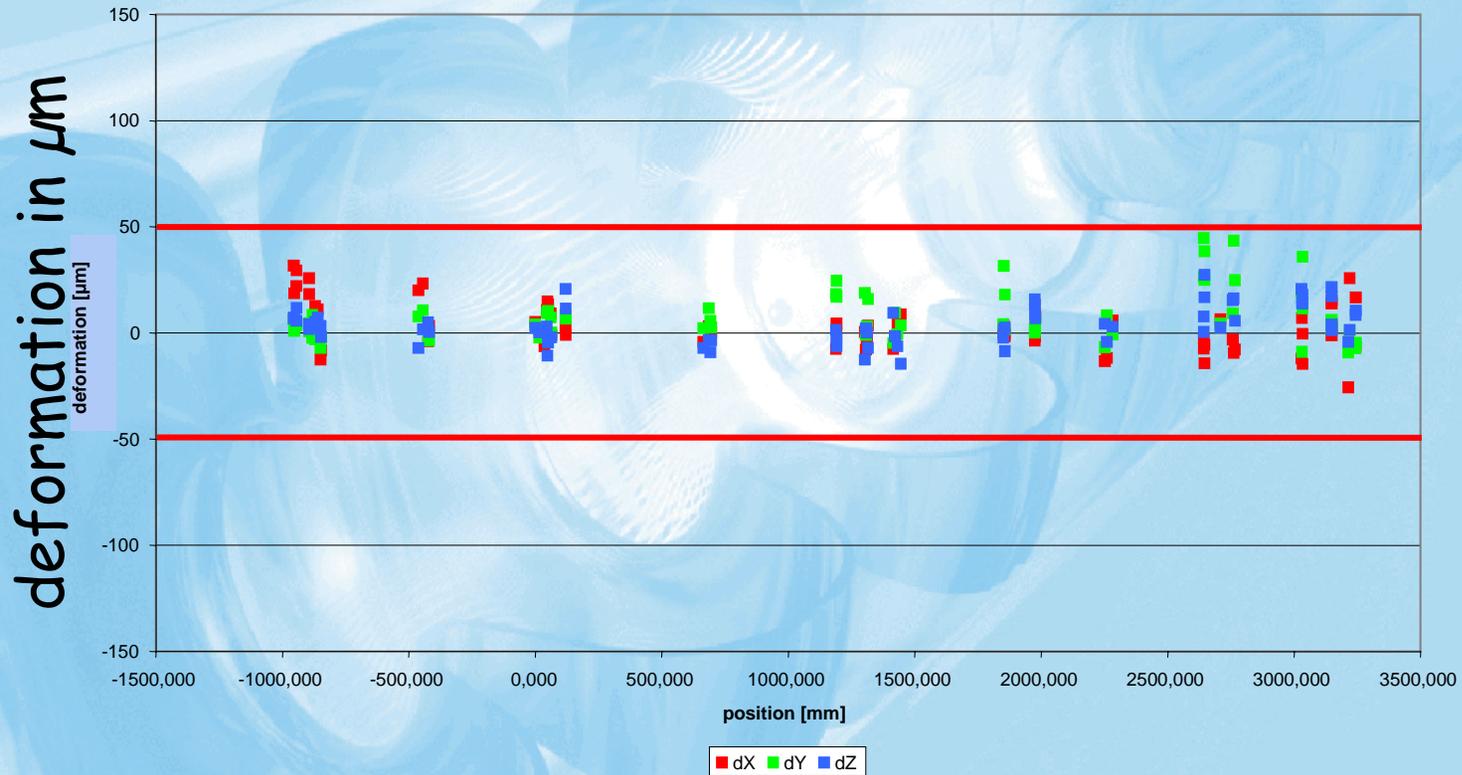
if it wouldn't be for the transport to the tunnel...



Transport



difference: before craning - after craning (targets on girder & magnets)



Overall accuracy



Let's assume we can get the shifts during transport to better than $\sigma = 40\mu\text{m}$...

that gives us...

$$\sigma = 50\mu\text{m}$$

Pretty close...

recheck the numbers for transport with

- new (more inflexible) girder
- our own climatized hall



Summary



Girder bears no coordinate information

Girder is not aligned in the tunnel, but the „median straight line“ of the **magnets**

Transfer Measurement should be done directly on girder

Accuracy requirements are met, but will be hopefully improved with the final girder



Dynamic behavior



Contradicts with static requirements:

for best static stability connection
between magnets and girder must be stiff

for least vibrations (from floor) in the magnets
connection must be elastic



Modal analysis of girder system



Analysis on concrete stands & final stands

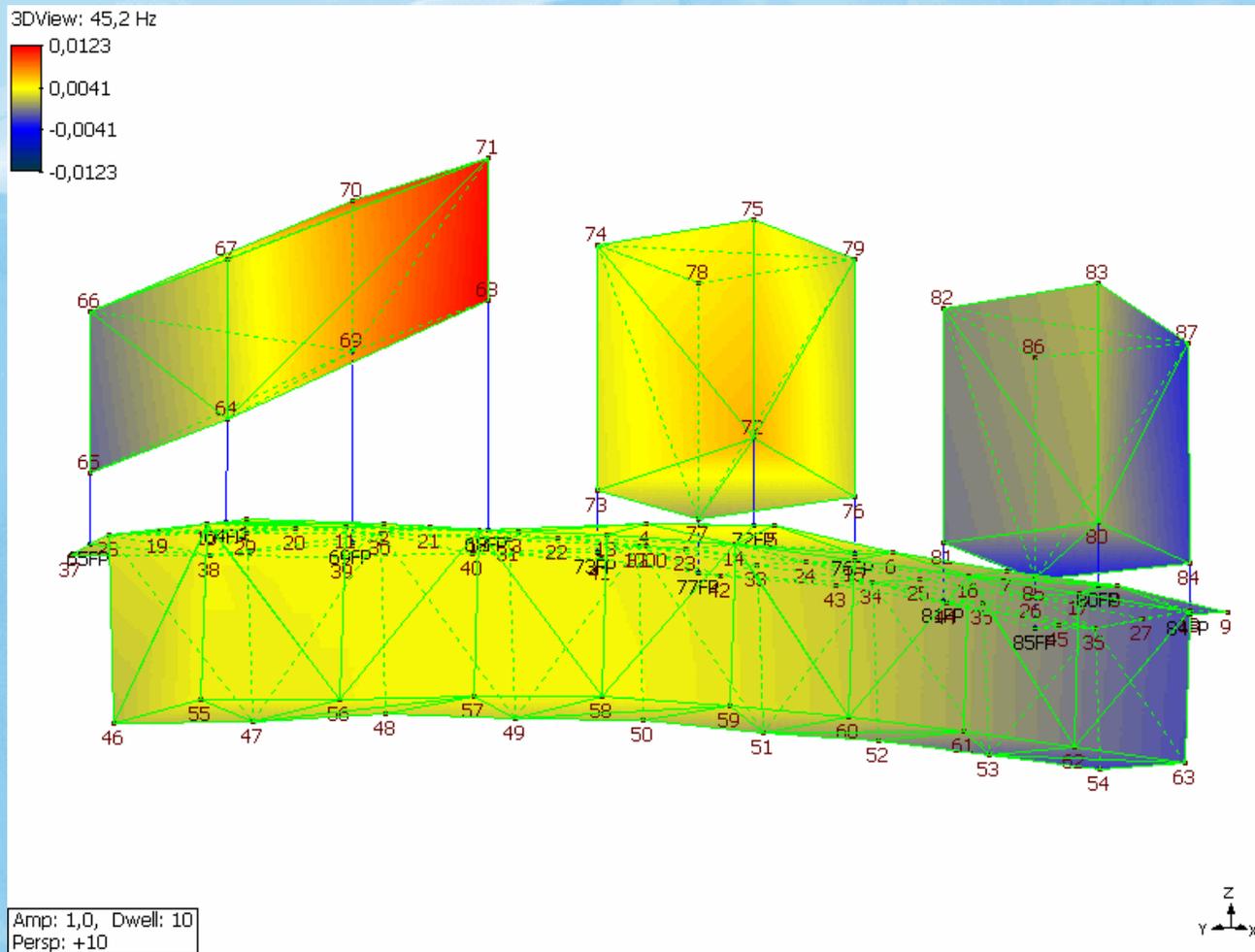
Measurement with accelerometers
and impact hammer



Modal analysis of girder system



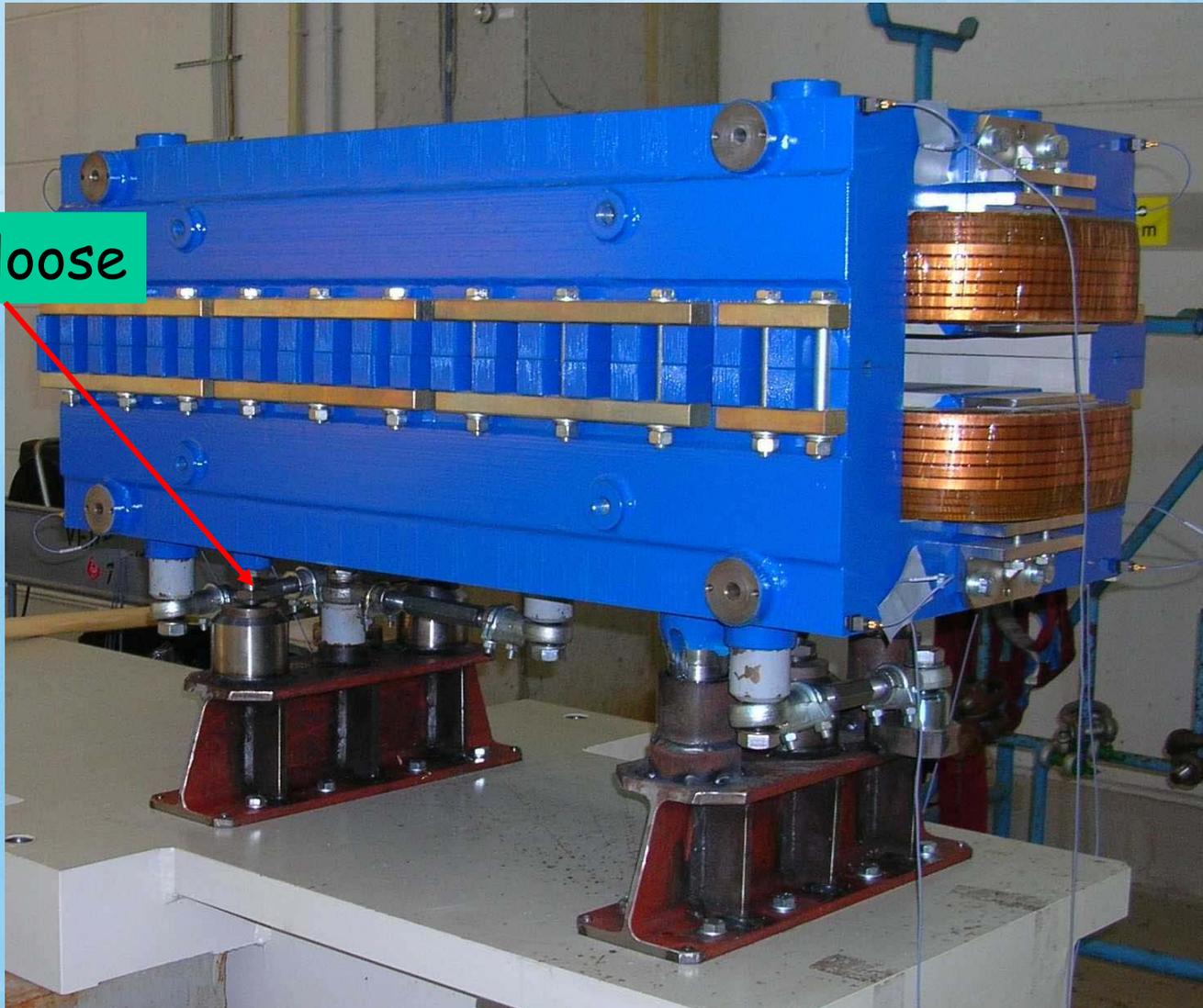
First eigenfrequency at 45Hz, Dipole loose



Modal analysis of girder system



Dipole loose



Modal analysis of girder system



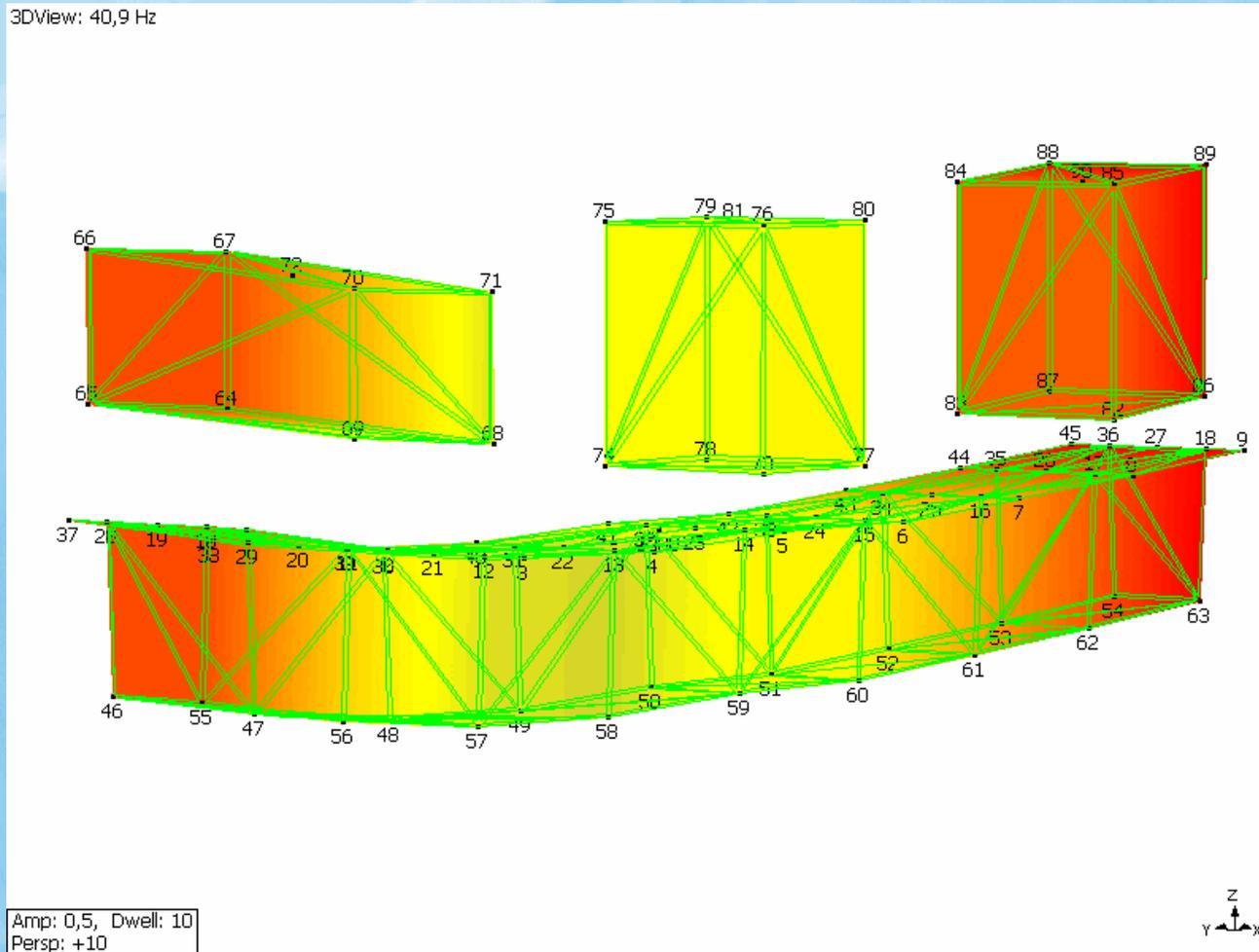
Dipole fixed



Modal analysis of girder system



First eigenfrequency at 41Hz, Dipole fixed



Modal analysis of girder system



Dipole loose



Modal analysis of girder system



Dipole fixed



Summary



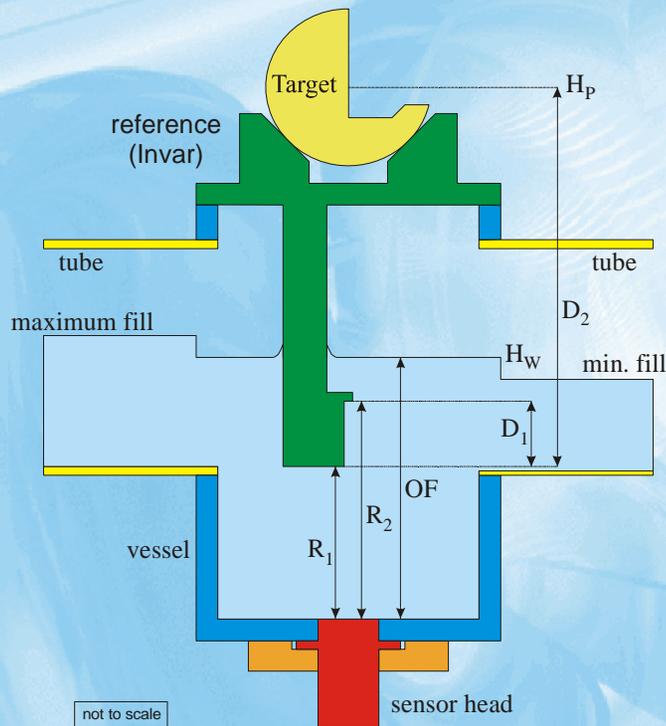
Modal analysis did help during the design of the girder

3D visualisation is important to convince other people

Analysis of Transfer Functions & Damping has still to be done



DESY-HLS with ultrasonic measurement and in-situ calibration



$$H_p = H_w + D_2 - D_1 \frac{OF - R_1}{R_2 - R_1}$$

unsatisfied with Krautkramer electronics

- complicated interface
- expensive
- but good accuracy



Build own electronics ...



Requirements:

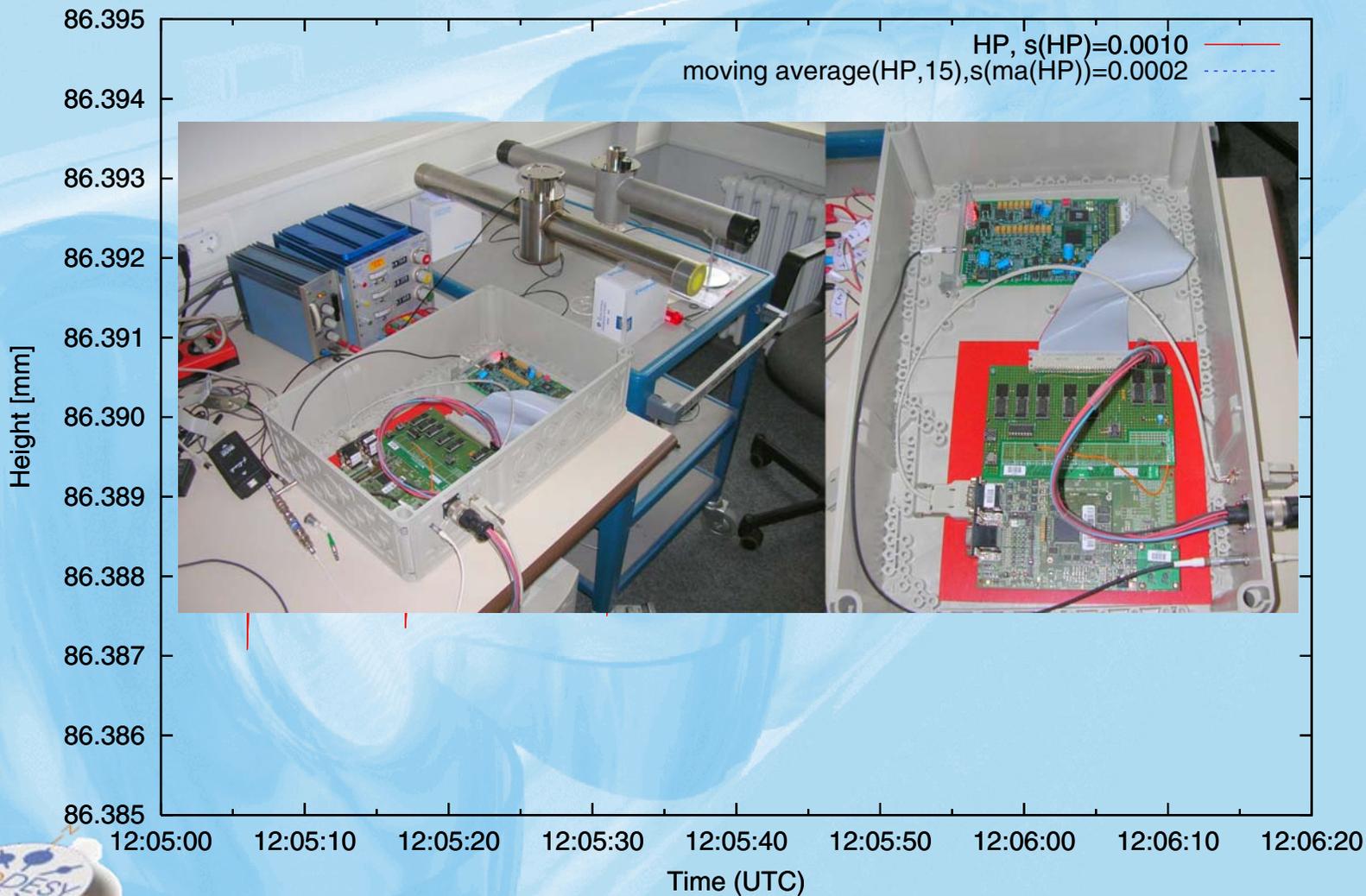
- up to four probes per device
- communication via CAN-open
- use proven and tested measurement pot with KK probe
- automatic measurement with failure detection
- transfer only results per default, but transfer raw data on demand
- cost efficient
- standard 19" crate
- accuracy better $2\mu\text{m}$ for resulting height



Prototype



DESY-HLS test of electronics



Pricing



Accuracy on the μm -level

One channel: 716€

Two channel: 928€ (470€ / channel)

Four channels: 1352€ (350€ / channel)

plus 1,2k€ / channel for measurement pot and probe

This is a preliminary and non-commercial price!



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Thanks
for your attention!

