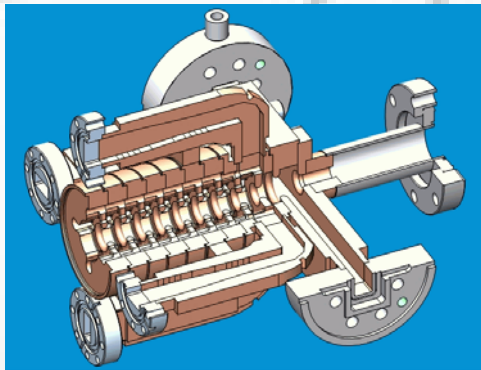
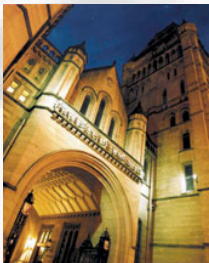
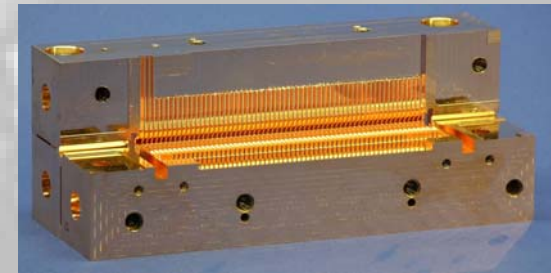


Wakefield Suppression for CLIC – A Manifold Damped and Detuned Structure



Roger M. Jones
**Cockcroft Institute and
The University of Manchester**



Wake Function Suppression for CLIC -Staff

- Roger M. Jones (Univ. of Manchester faculty)
- Alessandro D'Elia (Dec 2008, Univ. of Manchester PDRA based at CERN)
- Vasim Khan (Ph.D. student, Sept 2007)
- Part of EuCard (European Coordination for Accelerator Research and Development) FP7 NCLinac Task 9.2



V. Khan, CI/Univ. of Manchester Ph.D. student pictured at EPAC 08



A. D'Elia, CI/Univ. of Manchester PDRA based at CERN (former CERN Fellow).

- Collaborators: W. Wuensch, A. Grudiev (CERN)

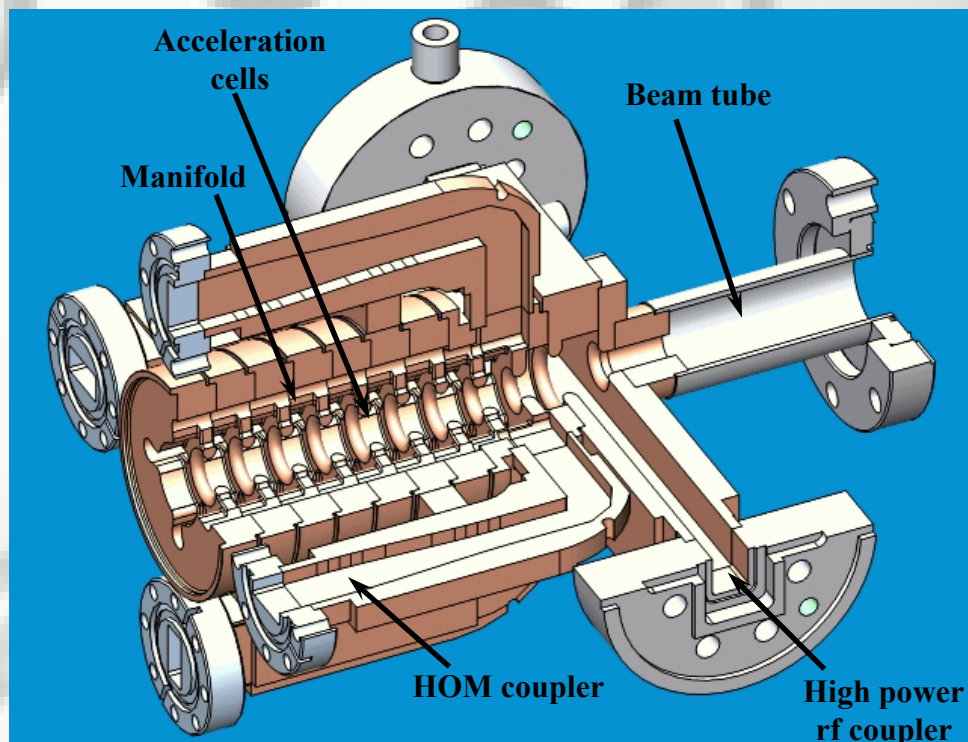
Three Main Parts:

1. **Introduction/features of manifold damped and detuned linacs.**
2. *Initial design indicating required bandwidth and necessary sigma of Gaussian*
3. *Design tied to CLIC_G –interleaving, zero-crossing*
4. *Design with relaxed parameters –modified bunch spacing, bunch population etc. Based on moderate damping on strong detuning*
5. **Concluding remarks**

1. Introduction –Present CLIC baseline vs. alternate DDS design

- The present CLIC structure relies on linear tapering of cell parameters and heavy damping with a Q of ~ 10 .
- Wake function suppression in entails heavy damping through waveguides and dielectric damping materials in relatively close proximity to accelerating cells.
- Alternative scheme, parallels the DDS, developed for the NLC/GLC entails:
 1. Detuning the dipole bands by forcing the cell parameters to have a precise spread in the frequencies –presently Gaussian K_{dn}/df - and interleaving the frequencies of adjacent structures.
 2. Moderate damping $Q \sim 500$

1. Features of CLIC DDS Accelerating Structure



- SLAC/KEK RDDS structure illustrates the essential features of the conceptual design
- Each of the cells is tapered –iris reduces with an erf-like distribution
- HOM manifold running alongside main structure removes dipole radiation and damp at remote location (4 in total)
- Each of the HOM manifolds can be instrumented to allow:
 - 1) Beam Position Monitoring
 - 2) Cell alignments to be inferred

1. CLIC Design Constraints

1) RF breakdown constraint

$$E_{sur}^{max} < 260MV / m$$

2) Pulsed surface heating

$$\Delta T^{max} < 56K$$

3) Cost factor

$$P_{in} \sqrt[3]{\tau_p} / C_{in} < 18MW \sqrt[3]{ns} / mm$$

Beam dynamics constraints

1) For a given structure, no. of particles per bunch N is decided by the $\langle a \rangle / \lambda$ and $\Delta a / \langle a \rangle$

2) Maximum allowed wake on the first trailing bunch

$$W_{t1} \leq \frac{6.667 \times 4 \times 10^9}{N} (V / pC / mm / m)$$

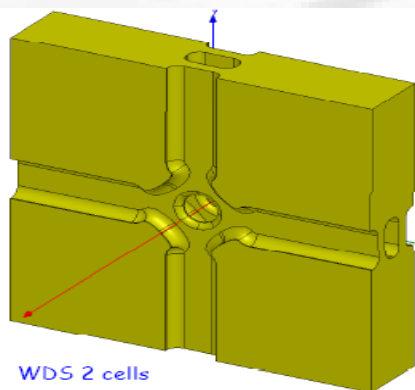
Wake experienced by successive bunches must also be below this criterion

Ref: Grudiev and Wuensch, *Design of an x-band accelerating structure for the CLIC main linacs, LINAC08*

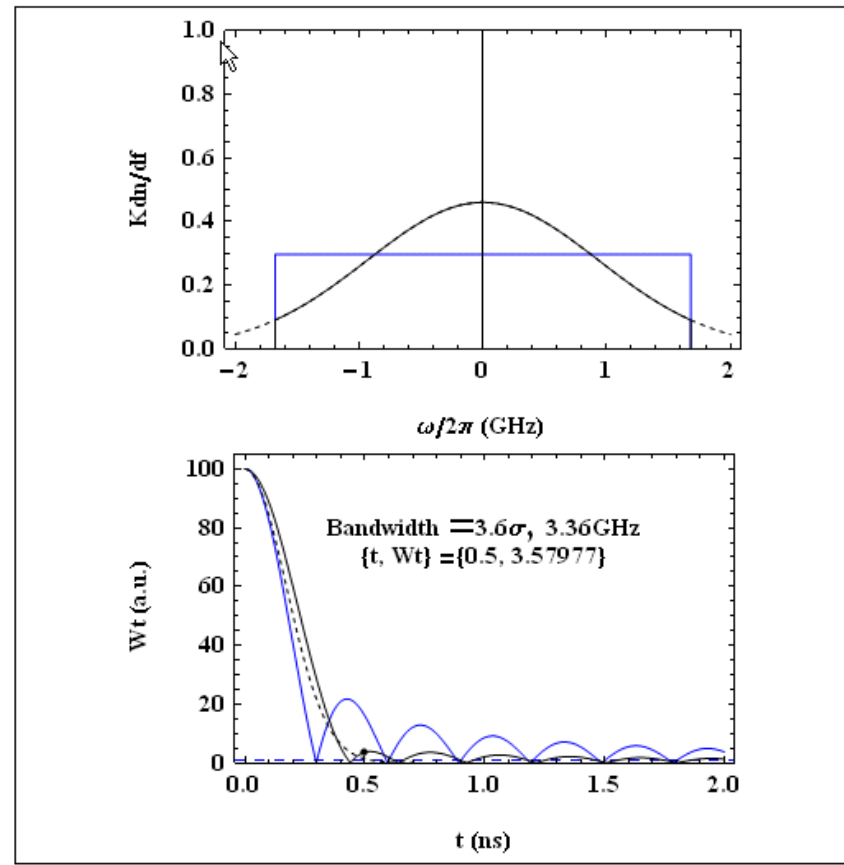
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1. Baseline CLIC_G Design

Structure	CLIC_G
Frequency (GHz)	12
Avg. Iris radius/wavelength $\langle a \rangle / \lambda$	0.11
Input / Output iris radii (mm)	3.15, 2.35
Input / Output iris thickness (mm)	1.67, 1.0
Group velocity (% c)	1.66, 0.83
No. of cells per cavity	24
Bunch separation (rf cycles)	6
No. of bunches in a train	312



Lowest dipole band:
 $\Delta f \sim 1\text{GHz}$
 $Q \sim 10$



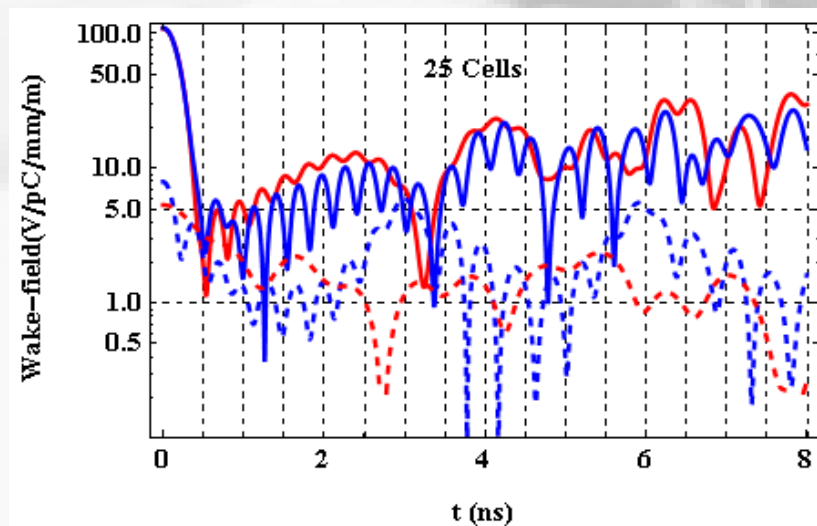
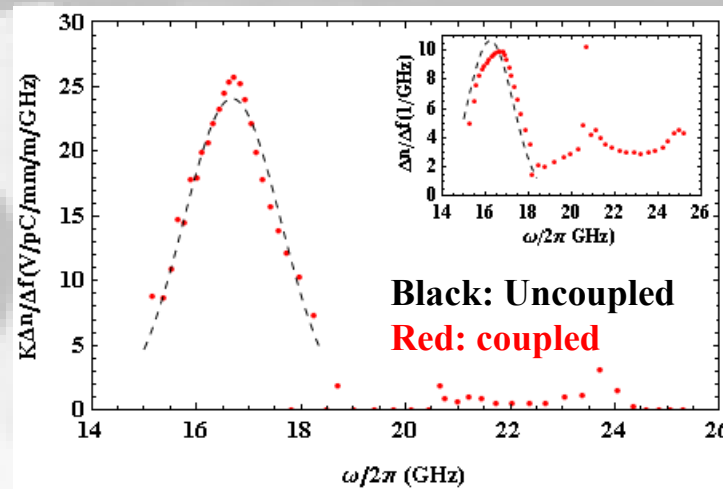
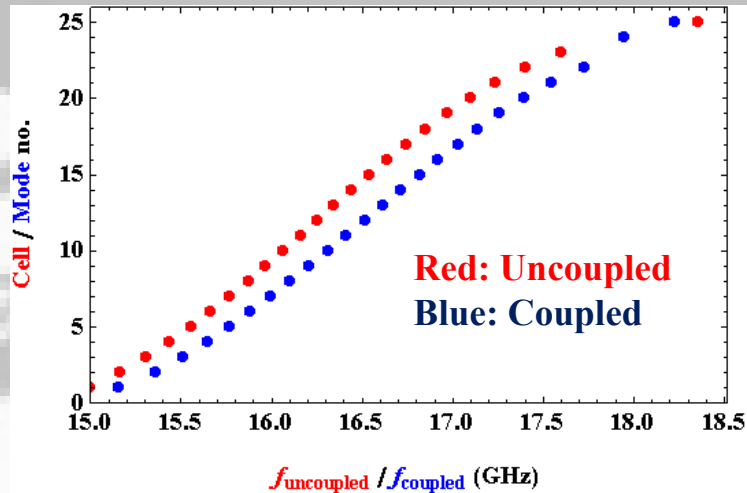
Truncated Gaussian :

$$W_t = 2K e^{-2(\sigma\pi t)^2} |\chi(t, \Delta f)|$$

where:
$$\chi(t, \Delta f) = \frac{\text{Re} \left\{ \text{erf} \left(\left[n_\sigma - 4i\pi\sigma t \right] / 2\sqrt{2} \right) \right\}}{\text{erf} \left(n_\sigma / 2\sqrt{2} \right)}$$

CLIC_DDS Uncoupled Design

2. Initial design for CLIC DDS



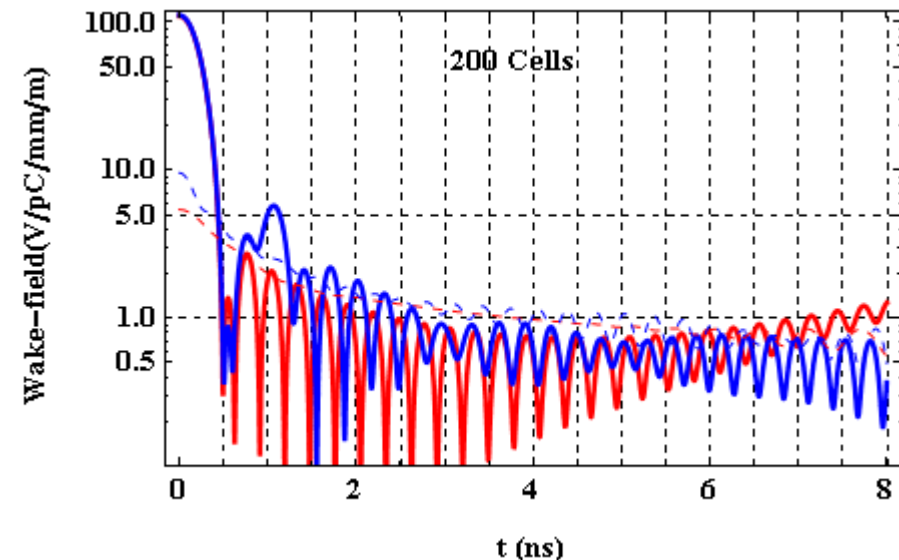
Solid curves: First dipole
Red: Uncoupled
Blue: Coupled
Dashed curves: second dipole

$$W_t(0) = 110 \text{ V/pc/mm/m}$$

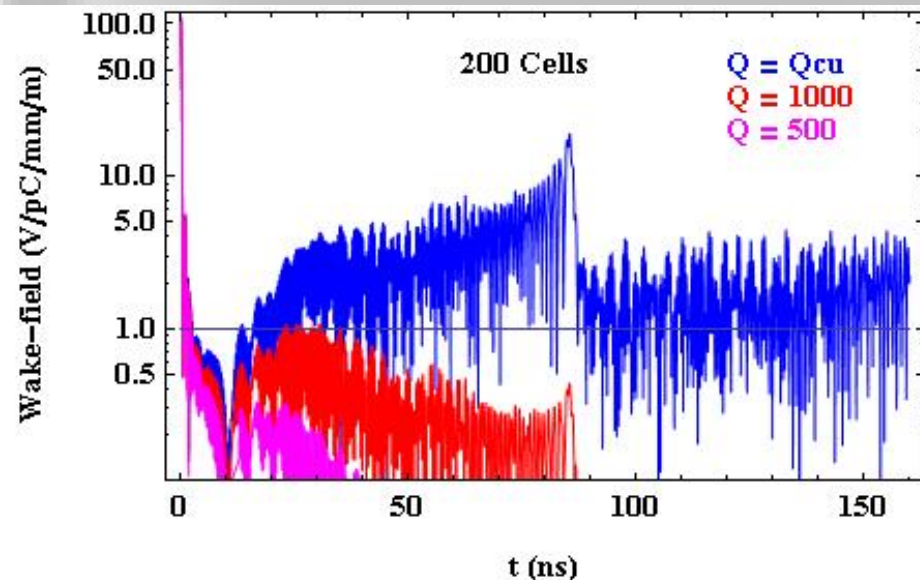
$$W_{t1} \sim 2 \text{ V/pc/mm/m}$$

Ref: Khan, Jones. Proc. of EPAC08

2. Initial design for CLIC DDS



First dipole **Uncoupled**, coupled.
Dashed curves: second dipole



- 8-fold interleaving employed
- Finite no of modes leads to a recoherance at ~ 85 ns.
- For a moderate damping Q imposed of ~ 1000 , amplitude of wake is still below 1V/pc/mm/m
- 3.3 GHz structure does satisfy the beam dynamics constraints
- However, it fails to satisfy RF breakdown constraints.

3. Gaussian distribution linked to CLIC_G parameters

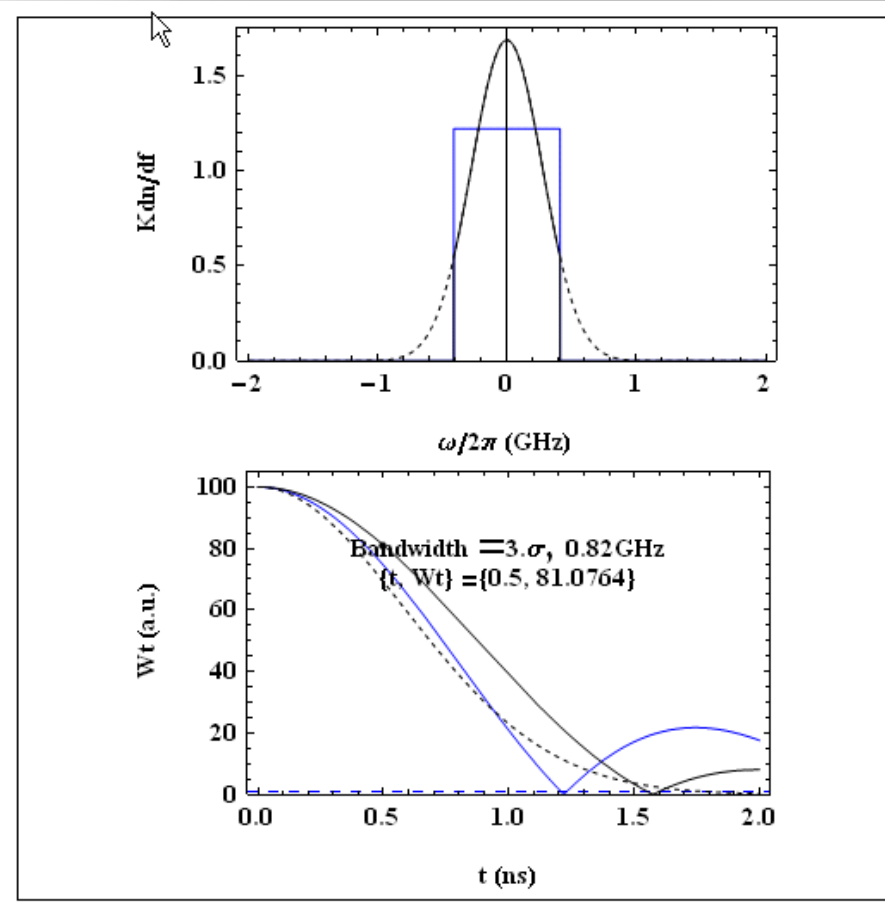
Cell	a (mm)	b (mm)	t (mm)	Vg/c (%)	f1 (GHz)
1	3.15	9.9	1.67	1.63	17.45
7	2.97	9.86	1.5	1.42	17.64
13	2.75	9.79	1.34	1.2	17.89
19	2.54	9.75	1.18	1.0	18.1
24	2.35	9.71	1.0	0.86	18.27

Uncoupled parameters:

$$\langle a \rangle / \lambda = 0.11$$

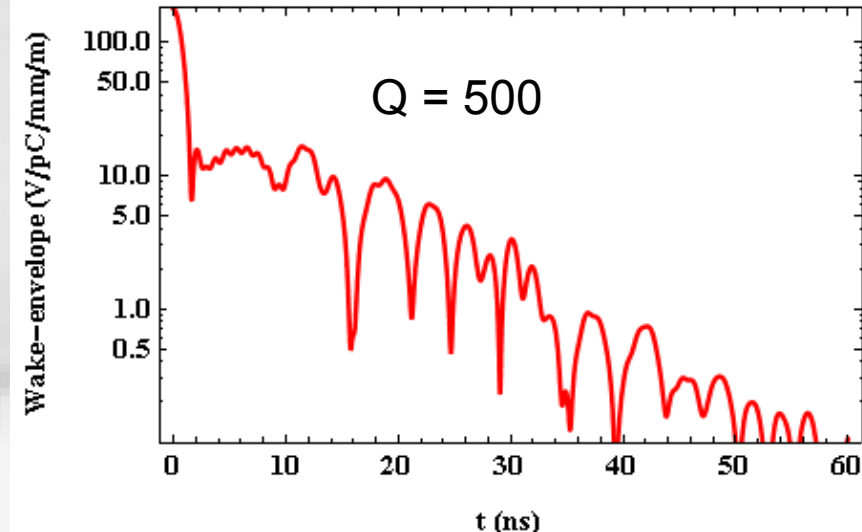
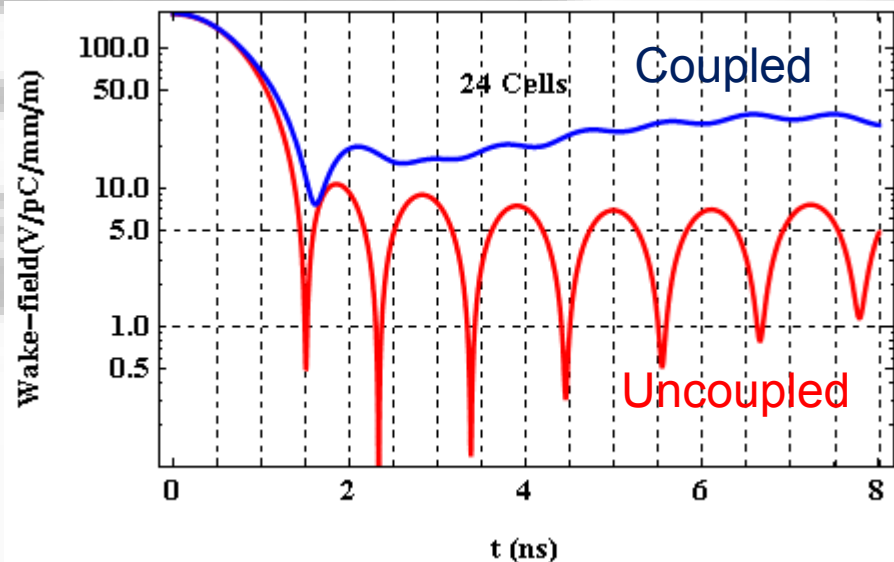
$$\Delta f = 3\sigma \sim 0.82 \text{ GHz}$$

$$\Delta f / \langle f \rangle = 4.5 \%$$

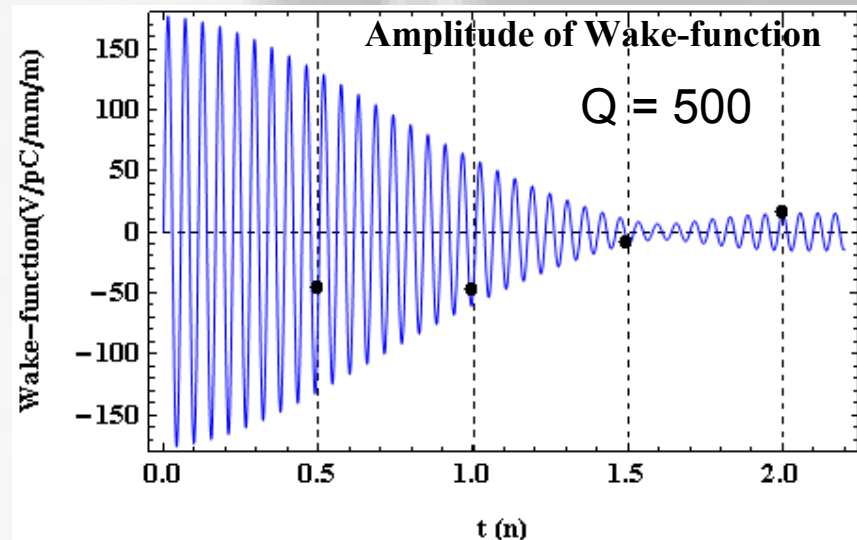


CLIC_DDS Uncoupled Design
tied to CLIC_G Parameters

3. Gaussian distribution linked to CLIC_G parameters



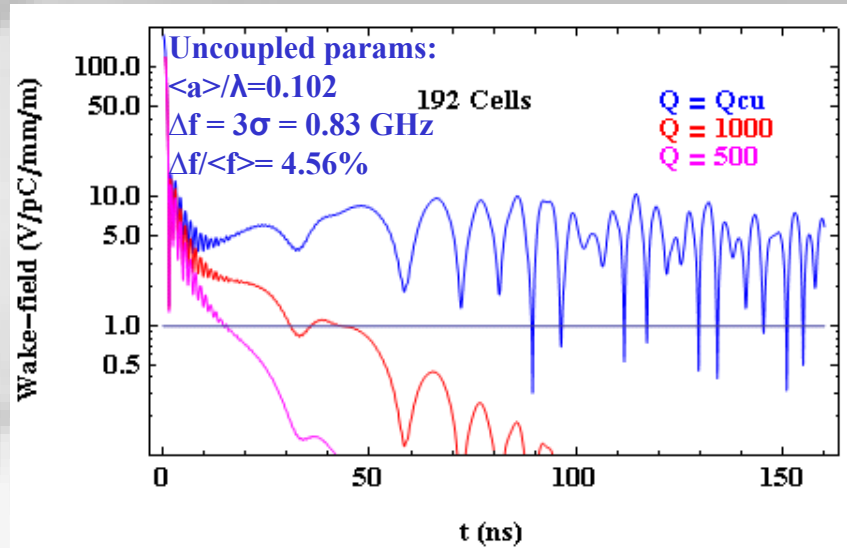
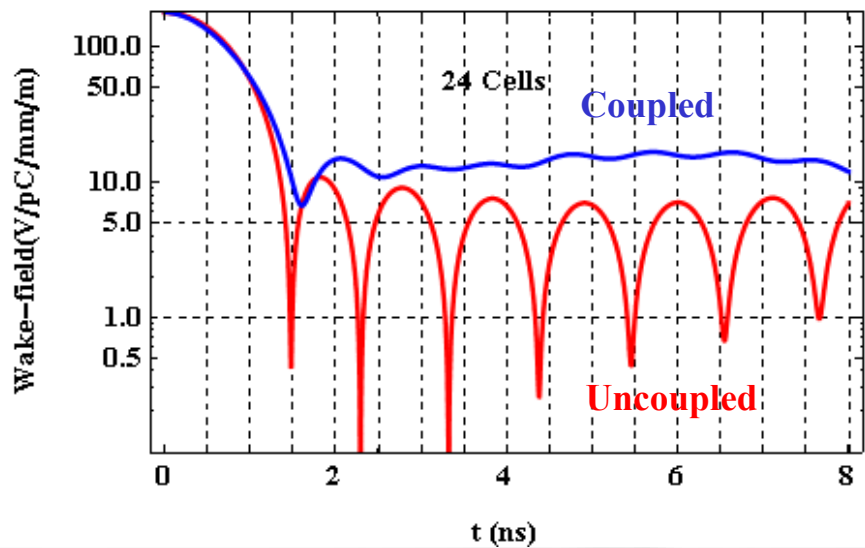
➤ Clearly the wake from the structure pinned to the CLIC_G parameters does not meet the design constraints!



Ref: Khan and Jones, Proc. PAC09

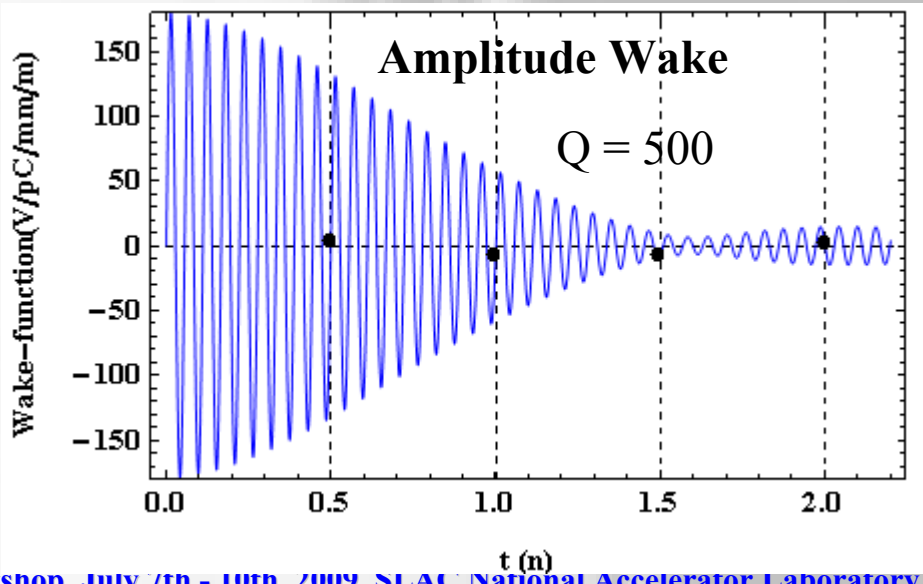
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3. Gaussian distribution linked to CLIC_G parameters

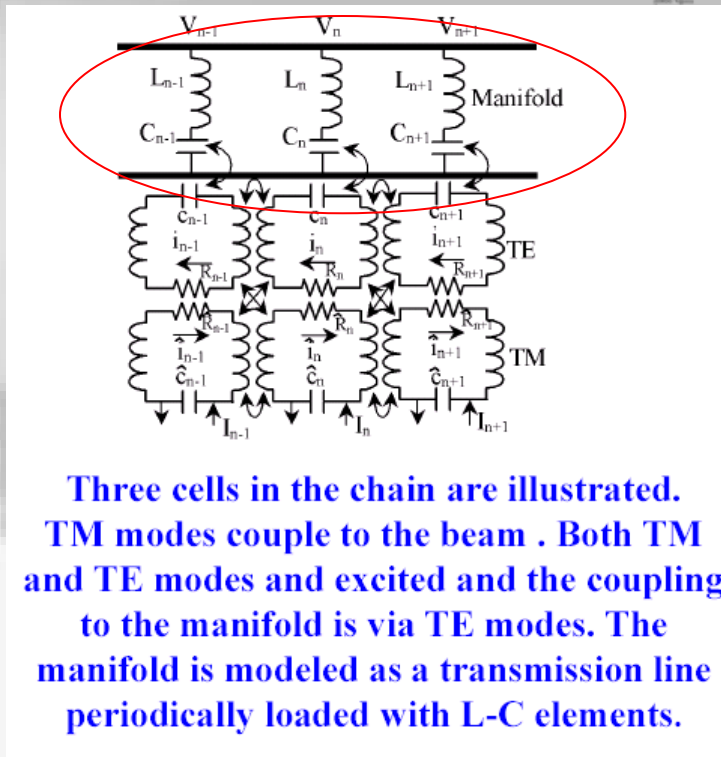
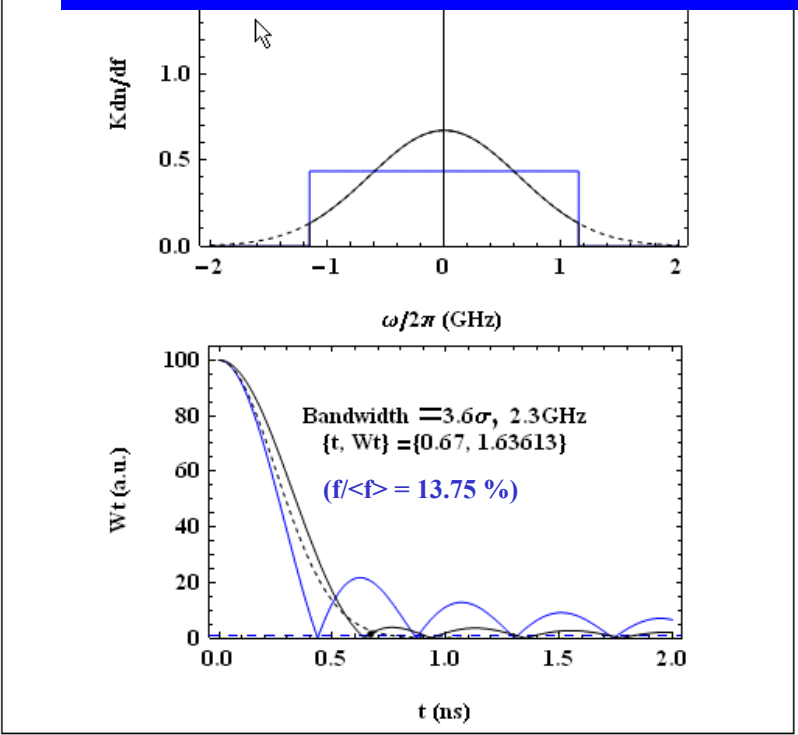


➤ Systematically shift cell parameters (aperture and cavity radius) in order to position bunches at the zero crossing in the amplitude of the wake function.

➤ Efficacy of the method requires a suite of simulations in order to determine the manufacturing tolerances.



4. Relaxed parameters tied to surface field constraints



Uncoupled parameters

Cell 1

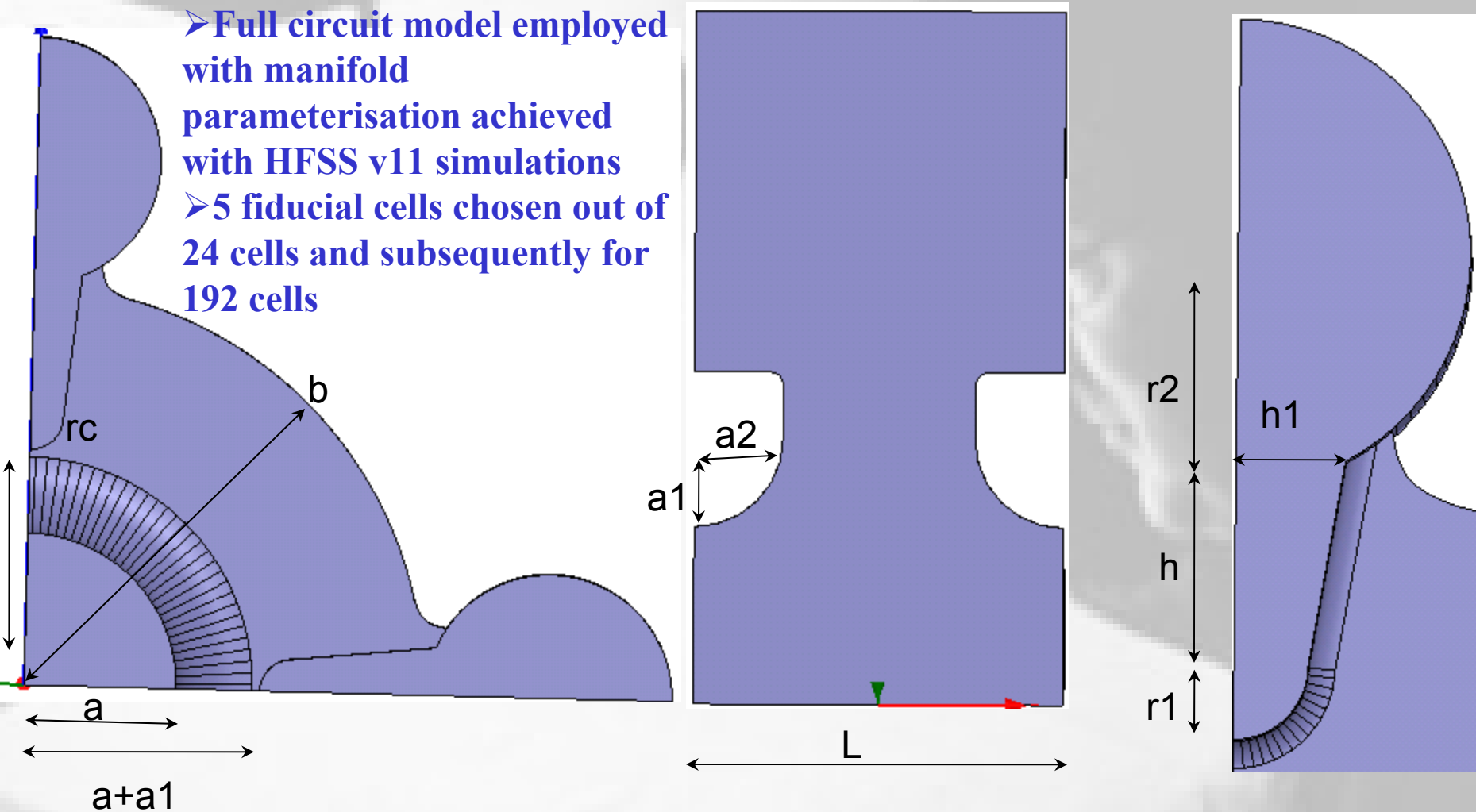
Cell 24

- Iris radius = 4.0 mm
- Iris thickness = 4.0 mm
- ellipticity = 1
- Q = 4771
- $R'/Q = 1,1640 \Omega/m$
- $vg/c = 2.13 \%$
- Iris radius = 2.3 mm
- Iris thickness = 0.7 mm
- ellipticity = 2
- Q = 6355
- $R'/Q = 20,090 \Omega/m$
- $vg/c = 0.9 \%$

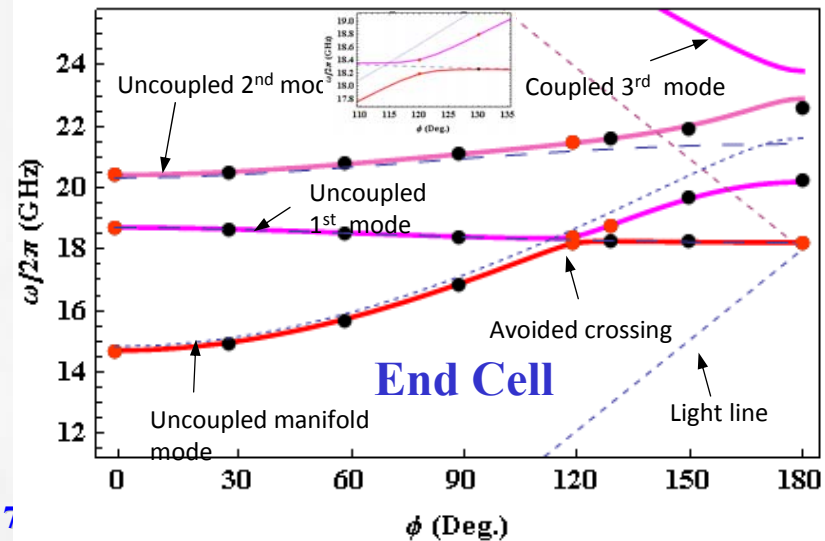
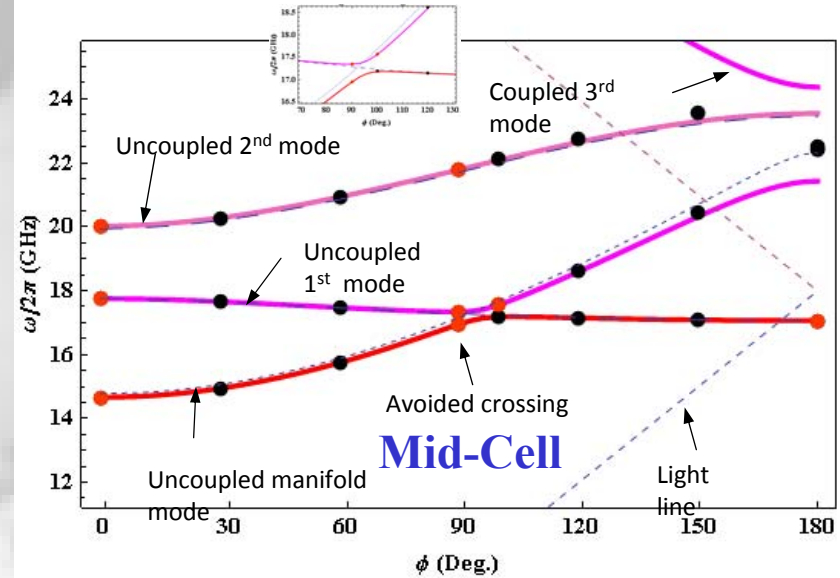
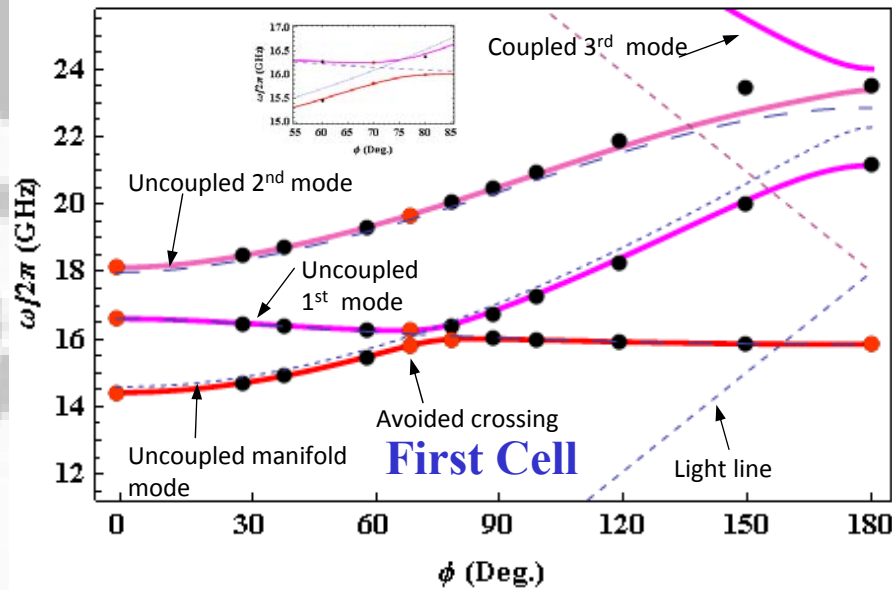
Cct Model Including Manifold-Coupling

4. Relaxed parameters tied to surface field constraints

- Full circuit model employed with manifold parameterisation achieved with HFSS v11 simulations
- 5 fiducial cells chosen out of 24 cells and subsequently for 192 cells

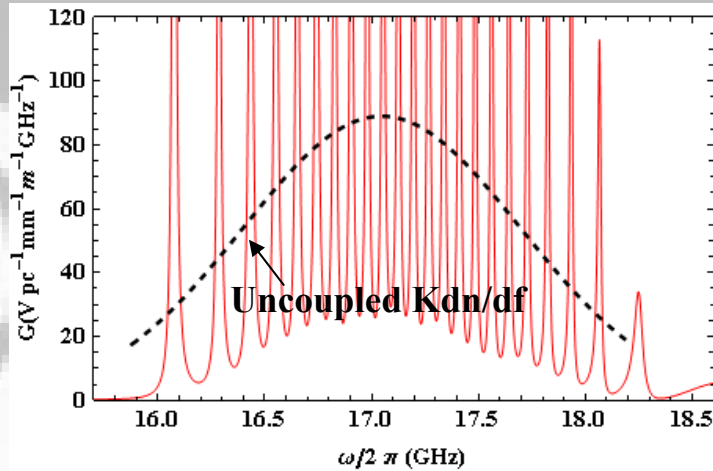


4. Relaxed parameters –full cct model

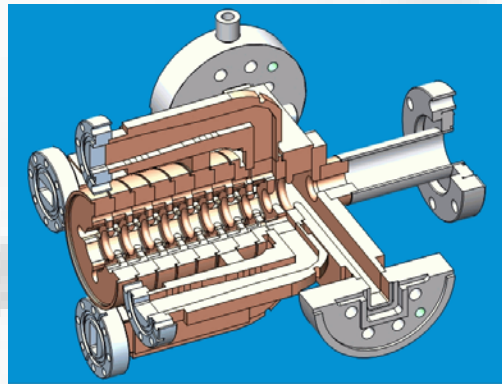


- Dispersion curves for select cells are displayed (red used in fits, black reflects accuracy of model)
- Provided the fits to the lower dipole are accurate, the wake function will be well-represented
- Spacing of avoided crossing (inset) provides an indication of the degree of coupling (damping Q)

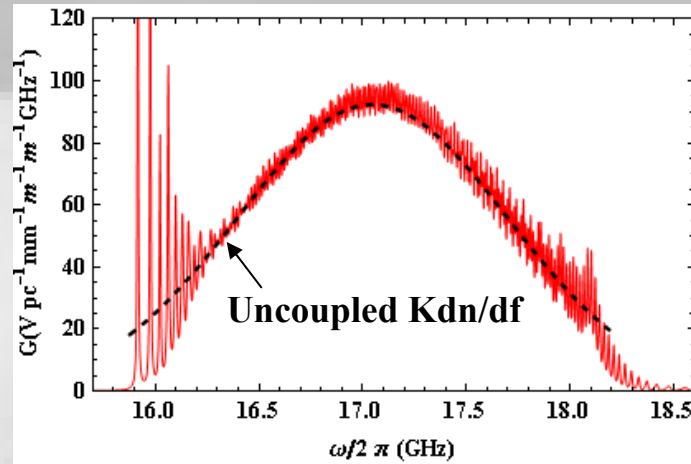
4. Relaxed parameters (RP)–Spectral fn.



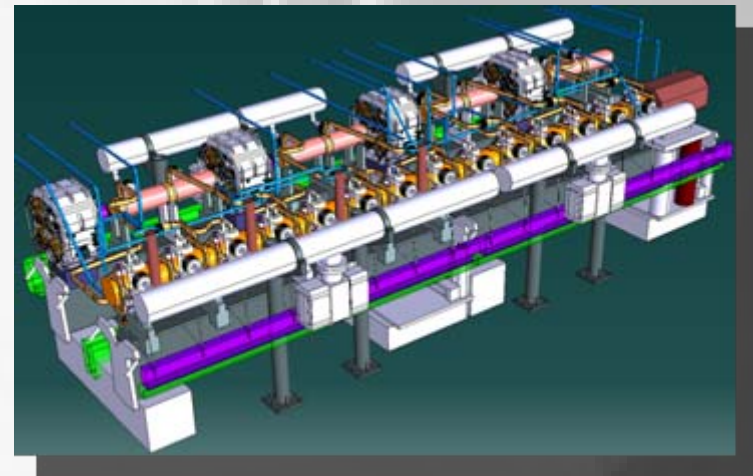
Single non-interleaved structure



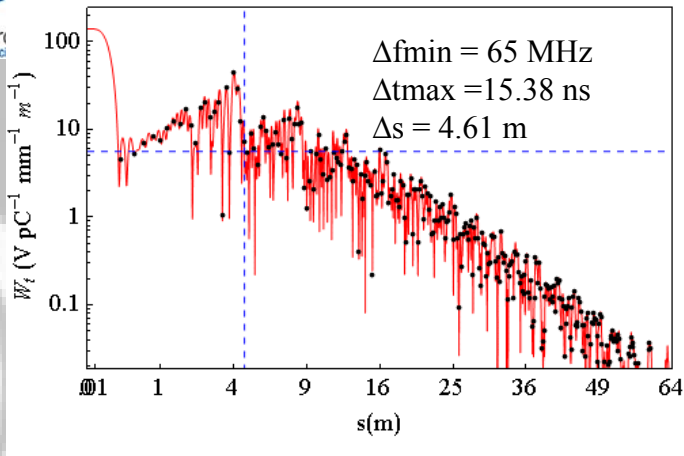
Potential Structure for CFT3 Module



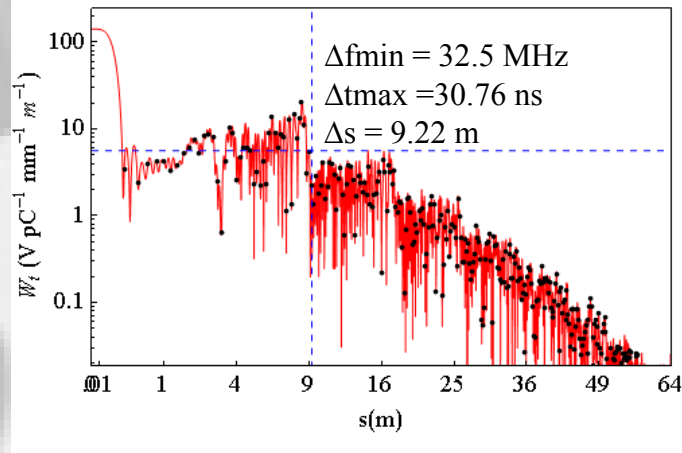
8-fold interleaved structure



Eight structures in each CFT3 module

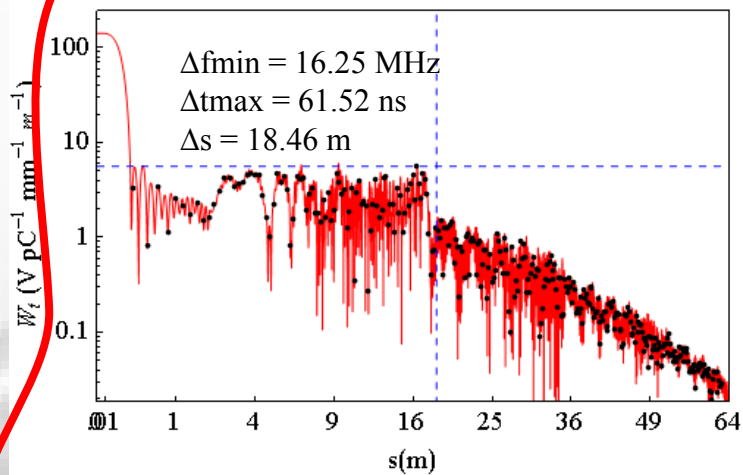


Single Structure Wake

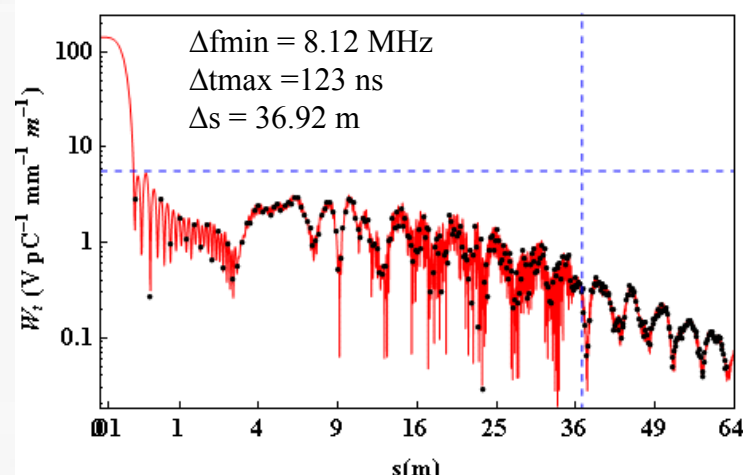


Two-fold interleaving

FAILS
design
criteria!



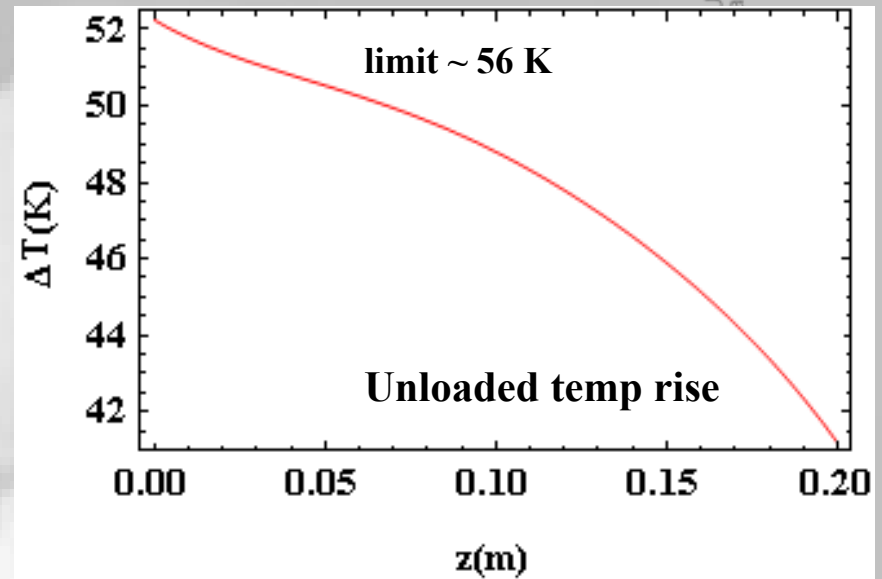
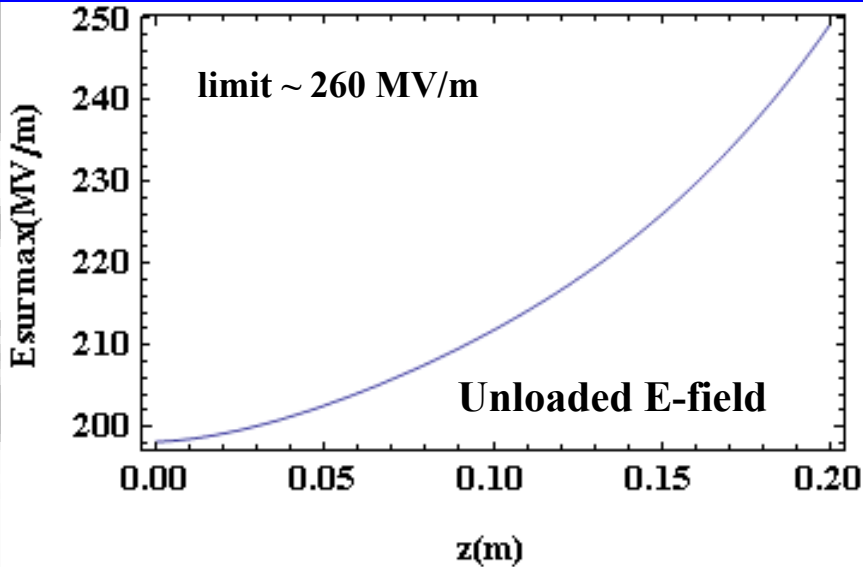
Four-fold interleaving



Eight-fold interleaving

MEETS
design
criteria!

4. Relaxed parameters (RP)–Efficiency Calc.



$$\tau_p = t_b + t_{fill} + t_r - \left(t_{fill} \frac{(1-pp)}{2} + t_r \left(1 - \frac{pp}{2} \right) \right) = 246 \text{ ns}$$

$$\Delta T \propto \sqrt{\tau_p}$$

$$\eta_{CLIC_DDS} = \frac{\text{beamenergy}}{\text{pulseenergy}} = \frac{I \langle E_{acc} \rangle L t_b}{P_{in} (t_b + t_r + t_{fill})}$$

$$\Rightarrow \boxed{\eta_{CLIC_DDS} = 23.4\%} \quad @ I = 1.13 \text{ A}$$

Initial, non-optimised!

$$P_{in} = 74.5 \text{ MW}$$

$$pp = \frac{P_{out}^L}{P_{out}^{UL}} = \frac{21.12}{37.77} = 0.56$$

$$t_b = \frac{8 \times 312}{11.9942} = 208.1 \text{ ns}$$

$$t_{fill} = 40 \text{ ns}$$

$$t_r \sim 23 \text{ ns}$$

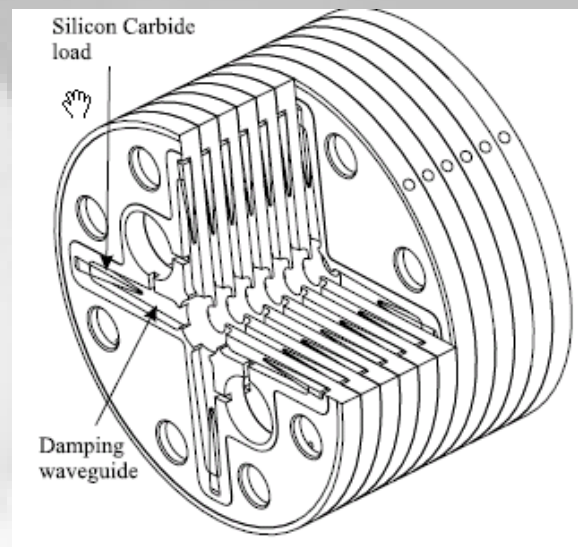
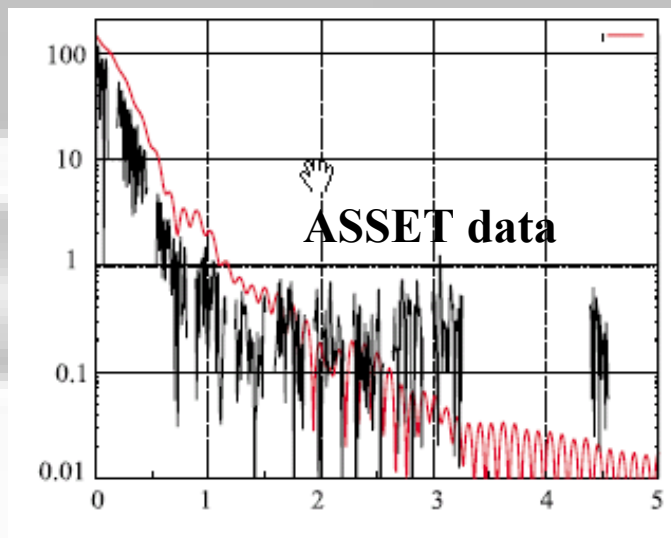
$$\boxed{\eta_{CLIC_G} = 27.7\%} \quad @ I = 1.19 \text{ A}$$

Ref: A. Grudiev, CLIC-ACE, JAN 08

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4. Concluding remarks

- The last two designs (ZC and RP) both meet both the beam dynamics and the breakdown constraints
- The design closely tied to the CLIC_G design requires the bunches to be located on the avoided crossing in the wake. This will need a comprehensive set of beam dynamics simulations in order to ensure realistic manufacturing tolerances are achievable.
- The modified design with relaxed parameters meets both constraints and in particular with full interleaving, experience with NLC/GLC structures leads us to conclude it *will lead to relaxed manufacturing tolerances*. These initial simulations are in the process of being optimised (efficiency enhancement calcs.)
- These new designs should be verified with experimental testing of wake function (revive ASSET??)

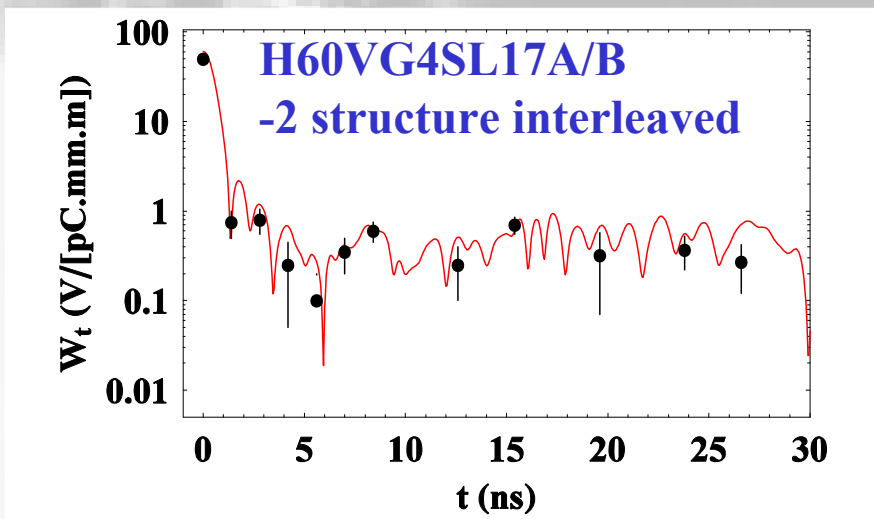
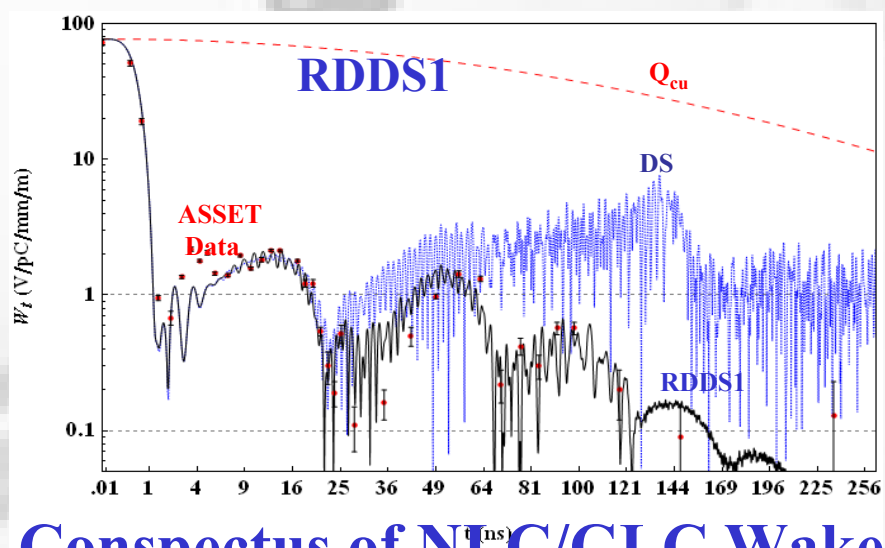
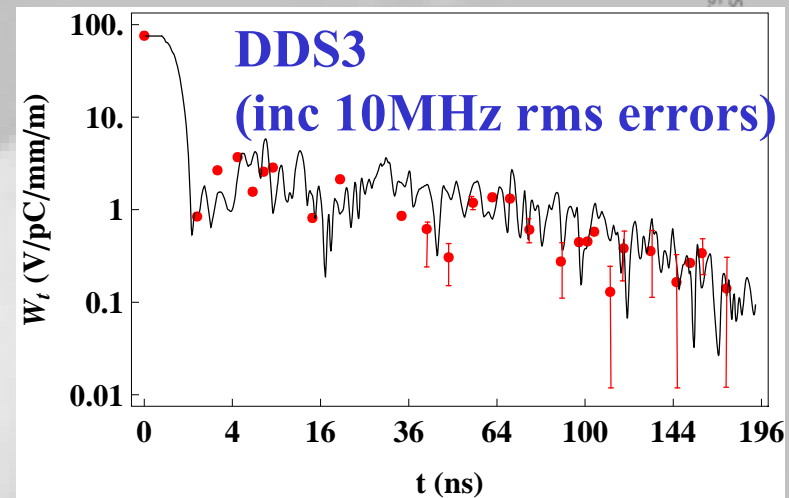
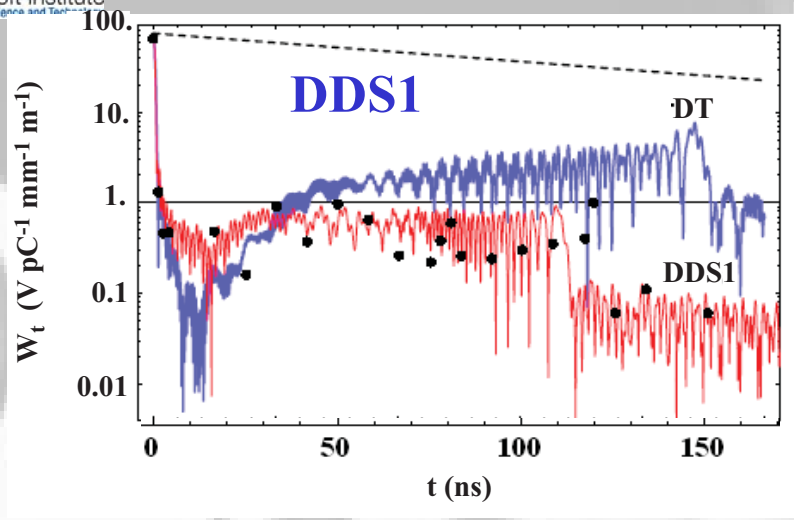


CLIC 30 GHz TDS Prediction vs Exp

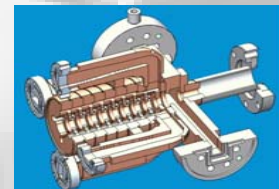
- Good agreement achieved up to ~ 2 ns
- Resonance, not included in prediction simulations, at 7.6 GHz, *external* to structure leads discrepancy between theory/exp.

Ref: I. Wilson et al., *Proceedings of the 2000 European Particle Accelerator Conference (EPAC00)*, Vienna, Austria, 2000

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Conspectus of NLC/GLC Wake Function Prediction and Measurement (ASSET dots)



Refs: 1. R.M. Jones, et al, *New J.Phys.*11:033013,2009. 2. R.M. Jones et al., *Phys.Rev.ST Accel. Beams* 9:102001, 2006.

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